

# Blended curves (§9.2)

- Assume degree 3
- Includes Hermite (§9.2.1), Bézier (§9.2.2), and others

$$Q(t) = \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix} = CT = \begin{bmatrix} a_x & b_x & c_x & d_x \\ a_y & b_y & c_y & d_y \\ a_z & b_z & c_z & d_z \end{bmatrix} \begin{bmatrix} t^3 \\ t^2 \\ t \\ 1 \end{bmatrix}$$

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- Assume degree 3
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$$Q(t) = \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix} = \begin{bmatrix} G_1 & G_2 & G_3 & G_4 \end{bmatrix} \begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \\ m_{41} & m_{42} & m_{43} & m_{44} \end{bmatrix} \begin{bmatrix} t^3 \\ t^2 \\ t \\ 1 \end{bmatrix}$$

# Hermite (§9.2.2)

- Geometry matrix
  - First two columns are endpoints
  - Next two columns are derivatives at those points

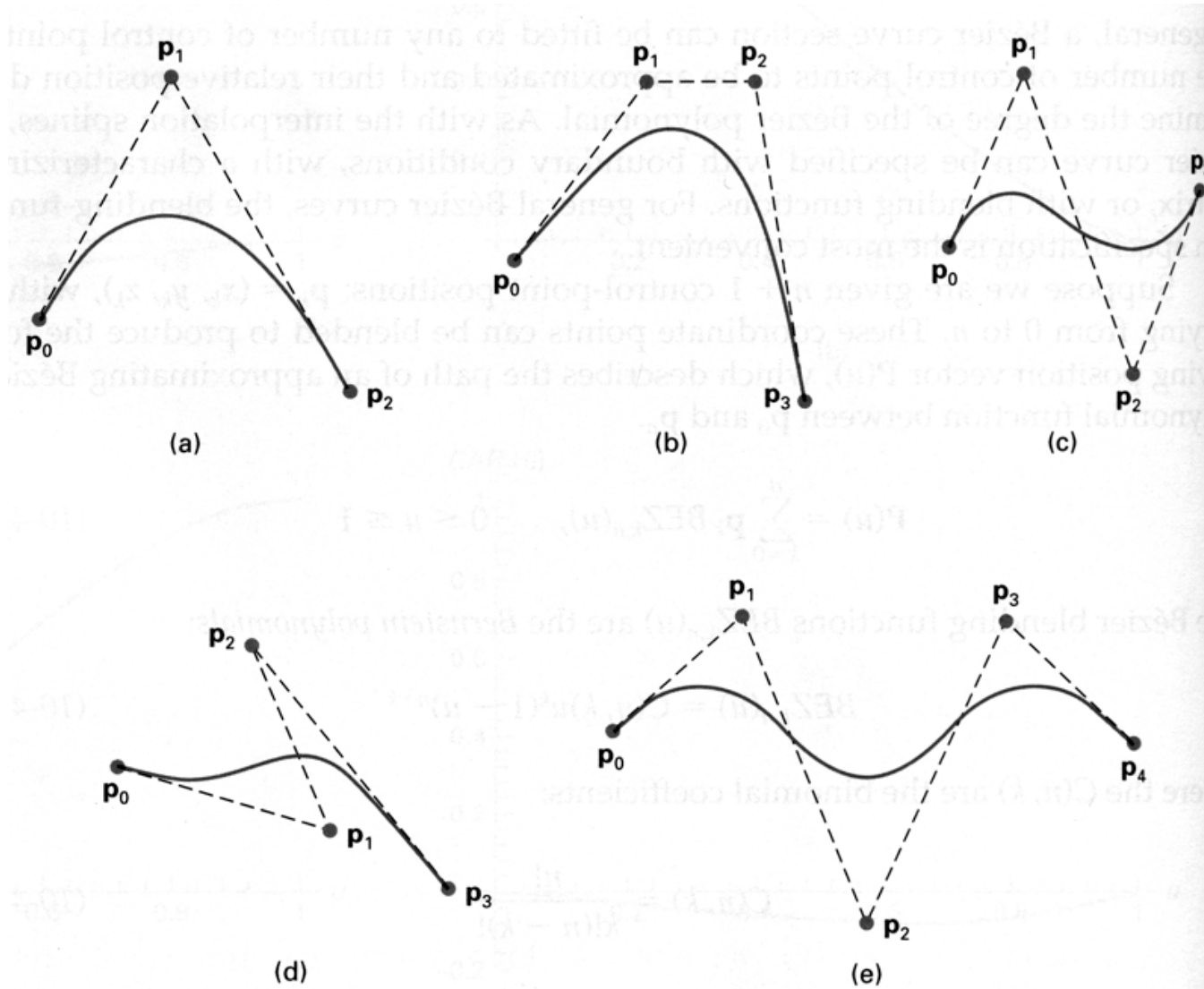
$$M_H = \begin{bmatrix} 2 & -3 & 0 & 1 \\ -2 & 3 & 0 & 0 \\ 1 & -2 & 1 & 0 \\ 1 & -1 & 0 & 0 \end{bmatrix}$$

Derivation?  
See page 333

## Bézier (§9.2.3)

- Curve goes through two control points
- Curve is adjusted by moving two (cubic case) other control points
- Tangent at endpoints is in direction of adjacent control point
- Curve lies in convex hull of all 4 (cubic case) control points.
  - First two columns are endpoints
  - Next two columns are derivatives at those points

# Example Bézier Curves



# Bézier (§9.2.2)

- Geometry matrix
  - First two columns are endpoints
  - Next two are like derivatives from the Hermite case, but are now defined by
$$R_1 = 3(P_2 - P_1)$$
$$R_2 = 3(P_4 - P_3)$$
  - Note that this gives our condition on endpoint tangents
  - Factor of 3 gives good “balance” in control point effect (see book exercise 9.9), and is needed to be consistent with other derivations (e.g., Bernstein polynomials, subdivision, etc).

$$\begin{aligned} R_1 &= 3(P_2 - P_1) \\ R_2 &= 3(P_4 - P_3) \end{aligned} \quad \text{Means that}$$

$$\begin{bmatrix} P_1 & P_4 & R_1 & R_2 \end{bmatrix} = \begin{bmatrix} P_1 & P_2 & P_3 & P_4 \end{bmatrix} \begin{bmatrix} 1 & 0 & -3 & 0 \\ 0 & 0 & 3 & 0 \\ 0 & 0 & 0 & -3 \\ 0 & 1 & 0 & 3 \end{bmatrix}$$

or

$$\begin{bmatrix} P_1 & P_4 & R_1 & R_2 \end{bmatrix} = \begin{bmatrix} P_1 & P_2 & P_3 & P_4 \end{bmatrix} M_{HB}$$

where

$$M_{HB} = \begin{bmatrix} 1 & 0 & -3 & 0 \\ 0 & 0 & 3 & 0 \\ 0 & 0 & 0 & -3 \\ 0 & 1 & 0 & 3 \end{bmatrix}$$

Recall Hermite

$$Q(t) = \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix} = \begin{bmatrix} P_1 & P_4 & R_1 & R_2 \end{bmatrix} M_H \begin{bmatrix} t^3 \\ t^2 \\ t \\ 1 \end{bmatrix}$$

From previous slide

$$\begin{bmatrix} P_1 & P_4 & R_1 & R_2 \end{bmatrix} = \begin{bmatrix} P_1 & P_2 & P_3 & P_4 \end{bmatrix} M_{HB}$$

So, for Bézier

$$Q(t) = \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix} = \begin{bmatrix} P_1 & P_2 & P_3 & P_4 \end{bmatrix} M_{HB} M_H \begin{bmatrix} t^3 \\ t^2 \\ t \\ 1 \end{bmatrix}$$



$$\text{Want } M_B \text{ in } Q(t) = \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix} = \begin{bmatrix} P_1 & P_2 & P_3 & P_4 \end{bmatrix} M_B \begin{bmatrix} t^3 \\ t^2 \\ t \\ 1 \end{bmatrix}$$

$$M_B = M_{HB} M_B$$

$$= \begin{bmatrix} 1 & 0 & -3 & 0 \\ 0 & 0 & 3 & 0 \\ 0 & 0 & 0 & -3 \\ 0 & 1 & 0 & 3 \end{bmatrix} \begin{bmatrix} 2 & -3 & 0 & 1 \\ -2 & 3 & 0 & 0 \\ 1 & -2 & 1 & 0 \\ 1 & -1 & 0 & 0 \end{bmatrix}$$

$$= \begin{bmatrix} -1 & 3 & -3 & 1 \\ 3 & -6 & 3 & 0 \\ -3 & 3 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$

## Bézier in standard form (summary)

$$Q(t) = \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix} = [P_1 \quad P_2 \quad P_3 \quad P_4] M_B \begin{bmatrix} t^3 \\ t^2 \\ t \\ 1 \end{bmatrix}$$

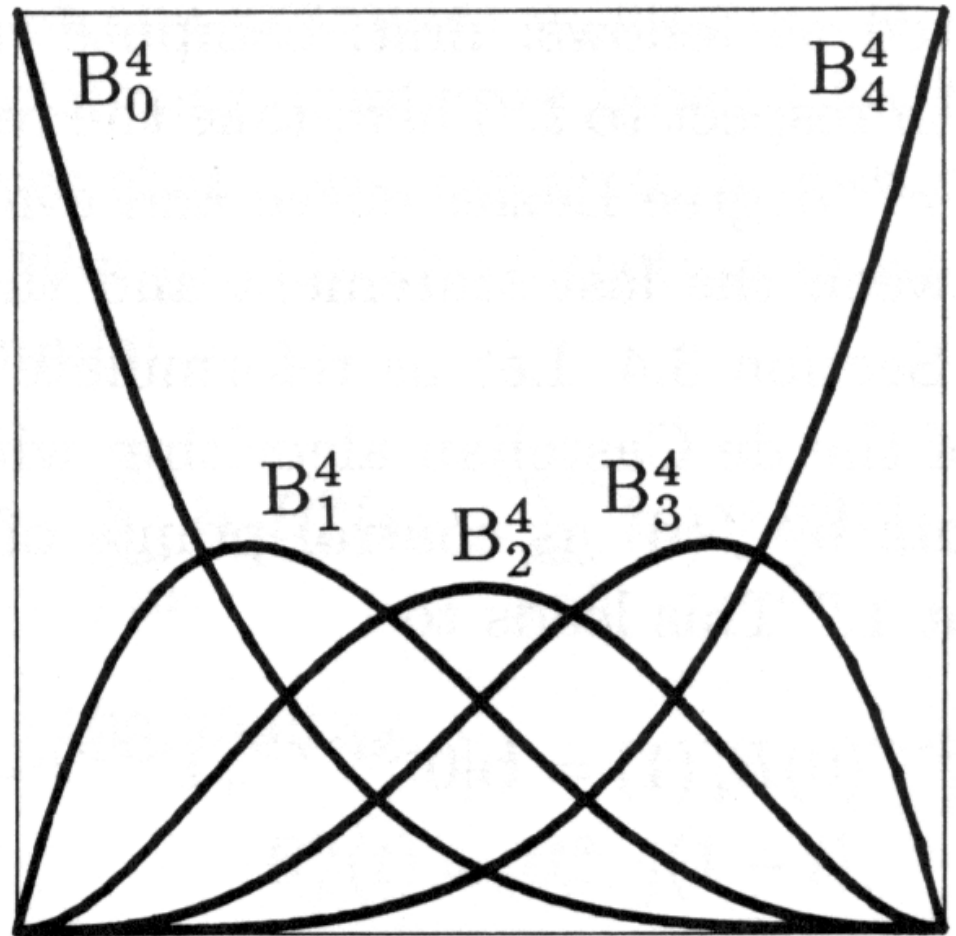
$$M_B = \begin{bmatrix} -1 & 3 & -3 & 1 \\ 3 & -6 & 3 & 0 \\ -3 & 3 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$

# Bézier curves - II

- Blending functions are the Bernstein polynomials

$$c(t) = \sum_{i=0}^n p_i B_i^n(t)$$

$$B_i^n(t) = \binom{n}{i} t^i (1-t)^{n-i}$$

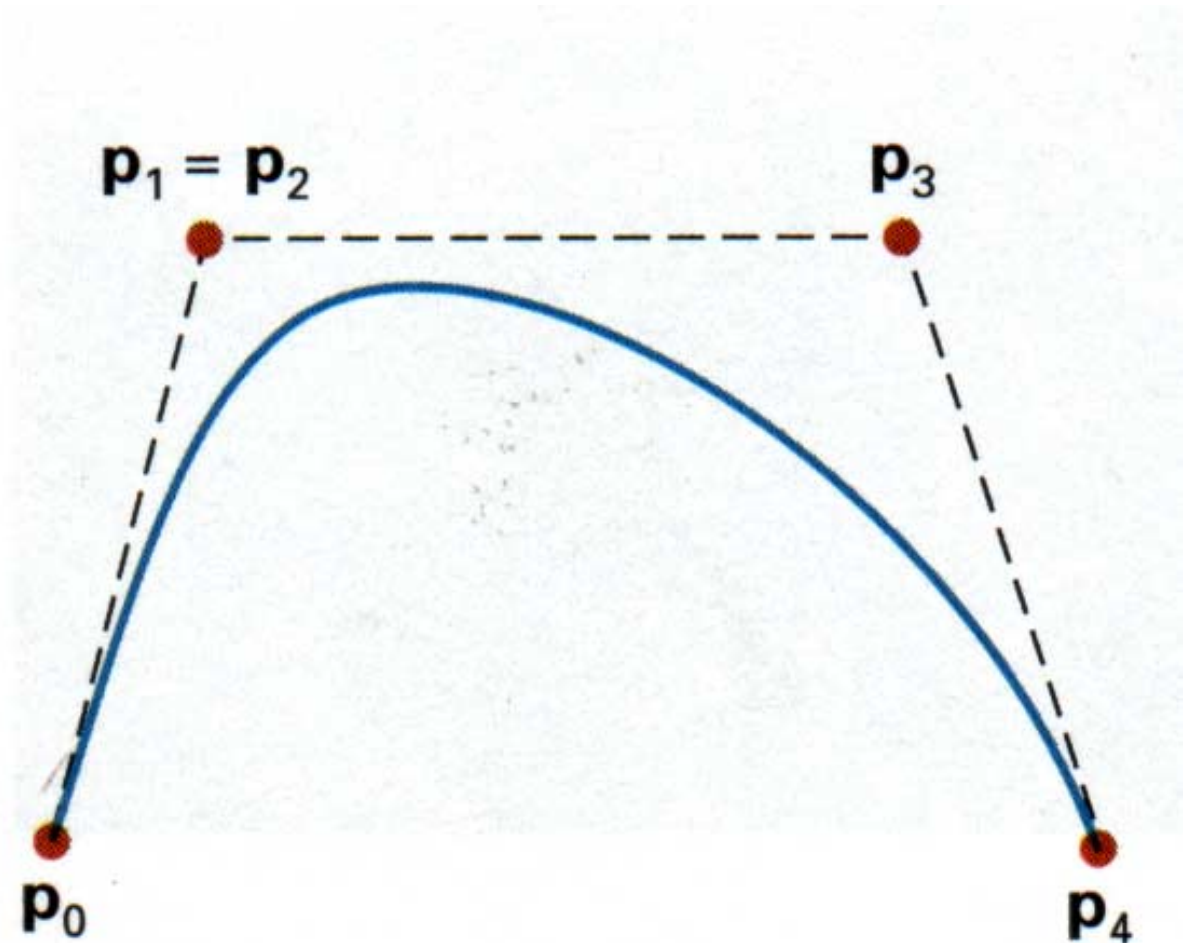


# Bézier curves - III

- Bernstein polynomials have several important properties
  - they sum to 1, hence curve lies within convex hull of control points
  - curve interpolates its endpoints
  - curve's tangent at start lies along the vector from  $p_0$  to  $p_1$
  - tangent at end lies along vector from  $p_{n-1}$  to  $p_n$

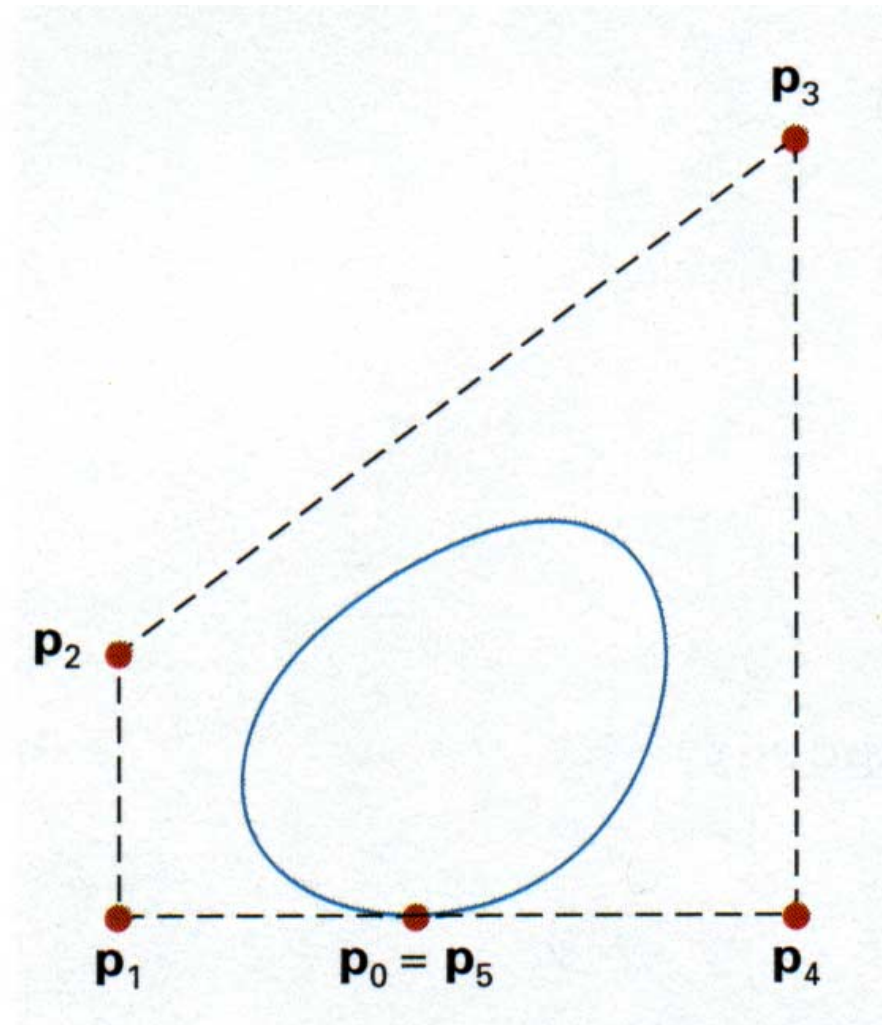
# Bézier curve tricks - I

- “Pull” a curve toward a control point by doubling the control point



# Bézier curve tricks-II

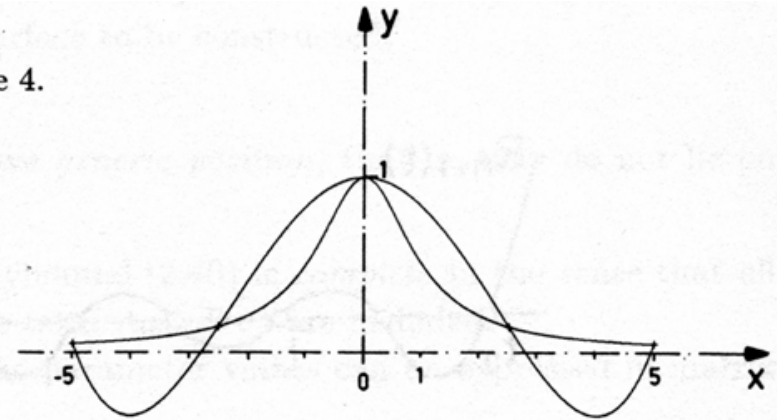
- Close the curve by making last point and first point coincident
  - curve has continuous tangent if first segment and last segment are collinear



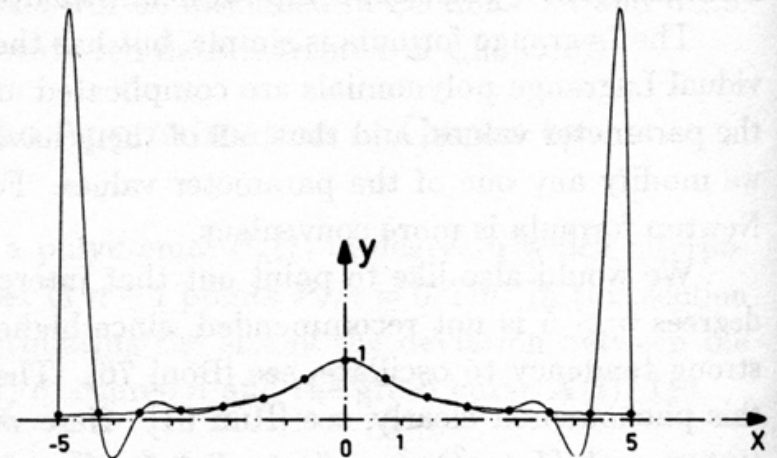
# Interpolating Splines

- Key idea:
  - high degree interpolates are badly behaved->
  - construct curves out of low degree segments

**Fig 2.16a.** Interpolation by a polynomial of degree 4.

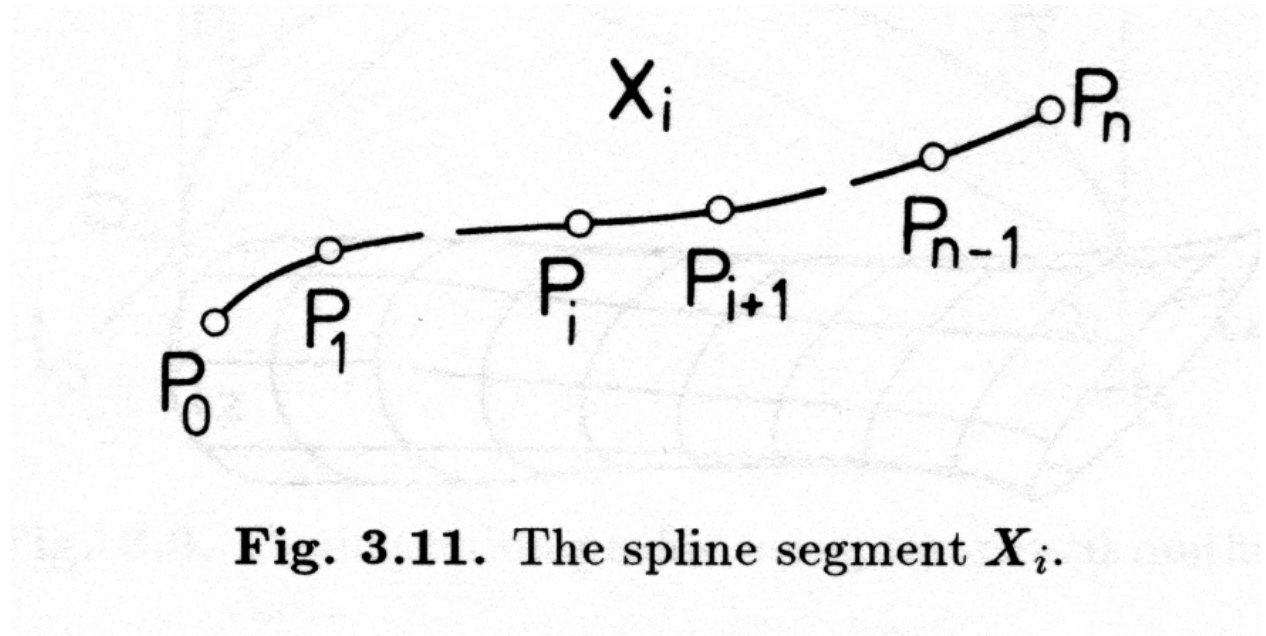


**Fig 2.16c.** Interpolation by a polynomial of degree 14.



# Interpolating Splines - II

- $n+1$  points;
- write derivatives  $X'$
- $X_i$  is spline for interval between  $P_i$  and  $P_{i+1}$



**Fig. 3.11.** The spline segment  $X_i$ .



# Interpolating Splines - II

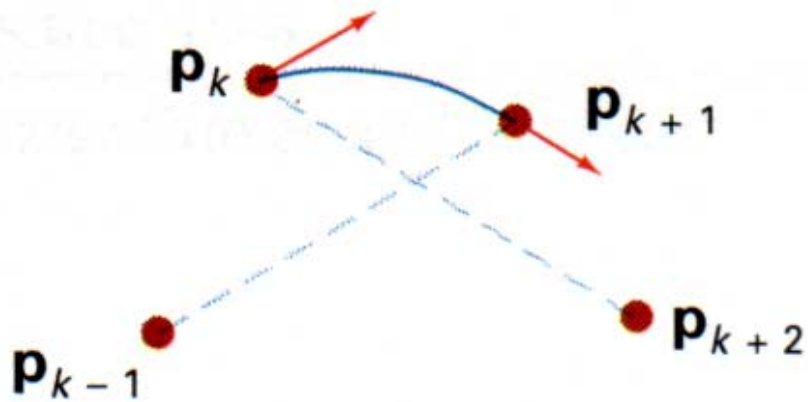
- Bolt together a series of Hermite curves with derivatives matching at joints (Knots).
- But where are the derivative values to come from?
  - Measurements
  - Combination of points (see cardinal splines--next topic)
  - Continuity considerations
  - Conventions for endpoints

- Cardinal splines

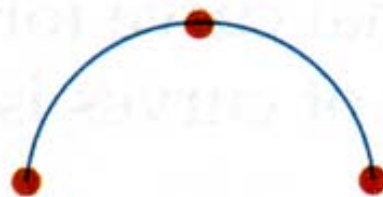
$$P'_k = \left(\frac{1}{2}\right)(1-t)(P_{k+1} - P_{k-1})$$

- t is “tension”
- still need to specify endpoint tangents
  - or use difference between first two, last two points

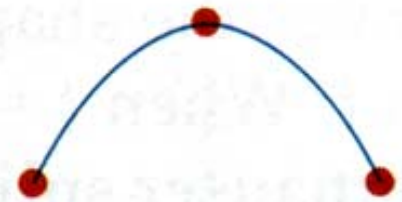
# Tension



- larger values of tension give tighter curves (limit is linear interpolate).



$t < 0$   
(Looser Curve)



$t > 0$   
(Tighter Curve)

# Interpolating Splines

- Intervals:

$$a = t_0 < t_1 < t_2 < \cdots < t_{N-1} < t_N = b.$$

$$\Delta t_i := t_{i+1} - t_i.$$

- $t$  values often called “knots”

- Spline form:

$$\begin{aligned} \mathbf{X}_i(t) &:= \mathbf{A}_i(t - t_i)^3 + \mathbf{B}_i(t - t_i)^2 + \mathbf{C}_i(t - t_i) + \mathbf{D}_i, \\ t &\in [t_i, t_{i+1}], \quad i = 0(1)N-1, \end{aligned}$$

# Continuity

- Require at endpoints:
  - endpoints equal
  - 1'st derivatives equal
  - 2'nd derivatives equal
- Now we get extra information from continuity (instead of tension equation, tangent measurements, etc)

$$\begin{array}{lll} \mathbf{X}_i(t_i) = \mathbf{X}_{i-1}(t_i) & \text{or} & \mathbf{X}_i(t_{i+1}) = \mathbf{X}_{i+1}(t_{i+1}), \\ \mathbf{X}'_i(t_i) = \mathbf{X}'_{i-1}(t_i) & \text{or} & \mathbf{X}'_i(t_{i+1}) = \mathbf{X}'_{i+1}(t_{i+1}), \\ \mathbf{X}''_i(t_i) = \mathbf{X}''_{i-1}(t_i) & \text{or} & \mathbf{X}''_i(t_{i+1}) = \mathbf{X}''_{i+1}(t_{i+1}). \end{array}$$

- From endpoint and 1'st derivative:

$$\begin{aligned} X_i(t_i) &= P_i = D_i, & X_i(t_{i+1}) &= P_{i+1} = A_i \Delta t_i^3 + B_i \Delta t_i^2 + C_i \Delta t_i + D_i, \\ X'_i(t_i) &= P'_i = C_i, & X'_i(t_{i+1}) &= P'_{i+1} = 3A_i \Delta t_i^2 + 2B_i \Delta t_i + C_i, \end{aligned}$$

- So that

$$\begin{aligned} A_i &= \frac{1}{(\Delta t_i)^3} [2(P_i - P_{i+1}) + \Delta t_i (P'_i + P'_{i+1})], \\ B_i &= \frac{1}{(\Delta t_i)^2} [3(P_{i+1} - P_i) - \Delta t_i (2P'_i + P'_{i+1})]. \end{aligned}$$

- Yielding:

$$\begin{aligned} X_i(t) &= \\ &P_i \left( 2 \frac{(t - t_i)^3}{(\Delta t_i)^3} - 3 \frac{(t - t_i)^2}{(\Delta t_i)^2} + 1 \right) + P_{i+1} \left( -2 \frac{(t - t_i)^3}{(\Delta t_i)^3} + 3 \frac{(t - t_i)^2}{(\Delta t_i)^2} \right) \\ &+ P'_i \left( \frac{(t - t_i)^3}{(\Delta t_i)^2} - 2 \frac{(t - t_i)^2}{\Delta t_i} + (t - t_i) \right) + P'_{i+1} \left( \frac{(t - t_i)^3}{(\Delta t_i)^2} - \frac{(t - t_i)^2}{\Delta t_i} \right) \end{aligned}$$

- Second Derivative:

$$X_i''(t) = 6P_i \left( \frac{2(t-t_i)}{(\Delta t_i)^3} - \frac{1}{(\Delta t_i)^2} \right) + 6P_{i+1} \left( -2\frac{(t-t_i)}{(\Delta t_i)^3} + \frac{1}{(\Delta t_i)^2} \right) \\ + 2P_i' \left( 3\frac{(t-t_i)}{(\Delta t_i)^2} - \frac{2}{\Delta t_i} \right) + 2P_{i+1}' \left( \frac{3(t-t_i)}{(\Delta t_i)^2} - \frac{1}{\Delta t_i} \right).$$

- Want:  $X_{i-1}''(t_i) = X_i''(t_i)$

$$\Delta t_i P_{i-1}' + 2(\Delta t_{i-1} + \Delta t_i) P_i' + \Delta t_{i-1} P_{i+1}' \\ = 3 \frac{\Delta t_{i-1}}{\Delta t_i} (P_{i+1} - P_i) + 3 \frac{\Delta t_i}{\Delta t_{i-1}} (P_i - P_{i-1}).$$

# Missing equations

- Recurrence relations represent  $d(n-1)$  equations in  $d(n+1)$  unknowns ( $d$  is dimension)
- We need to supply the derivative at the start and at the finish (or two equivalent constraints)
- Options:
  - second derivatives vanish at each end (natural spline)
  - give slopes at the boundary
    - vector from first to second, second last to last
    - parabola through first three, last three points
  - third derivative is the same at first, last knot

# B-splines - I

- Now consider stitching together curves which do not necessarily pass through the control points (i.e., back to blending functions).
- Local control
- Blending functions are non-zero over limited range--thus they are like “switches”
- In the simplest case of uniformly spaced control points, the blending functions will be shifted versions of the same function.



# B-splines - II

- Curve (general case):

$$X(t) = \sum_{k=0}^n P_k B_{k,d}(t)$$

- The “order”  $d$  is:

$$2 \leq d \leq n + 1$$

- Usual case:  $n$  is 4,  $d$  is 3.

# B-Spline Blending Functions (§9.2.5)

- Knots
  - parameter values where curve segments meet, as in Hermite example

$$(t_0, t_1, \dots, t_{n+d})$$

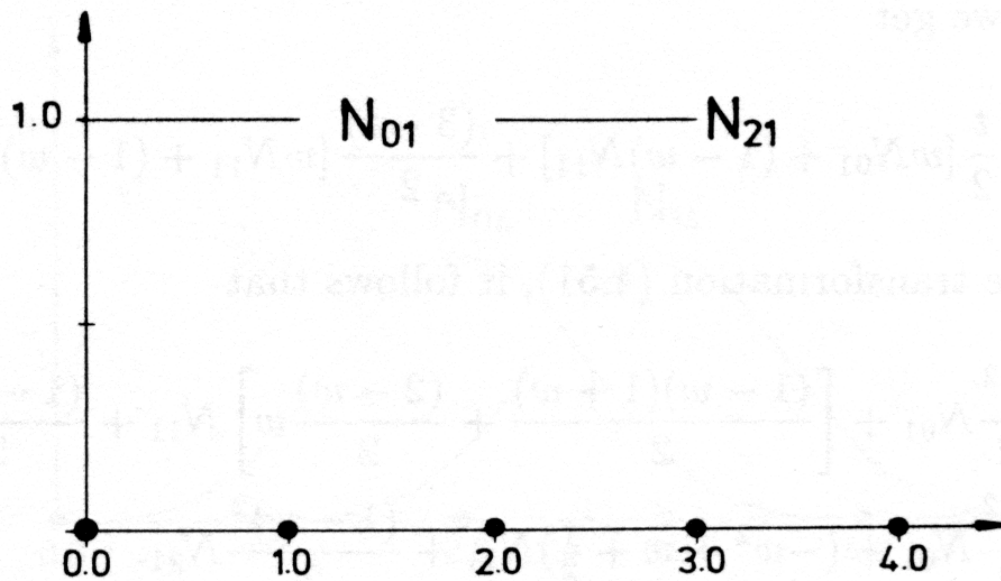
where  $t_0 \leq t_1 \leq \dots \leq t_{n+d}$

- Blending functions

$$B_{k,1}(t) = \begin{cases} 1 & t_k \leq t \leq t_{k+1} \\ 0 & \text{otherwise} \end{cases}$$

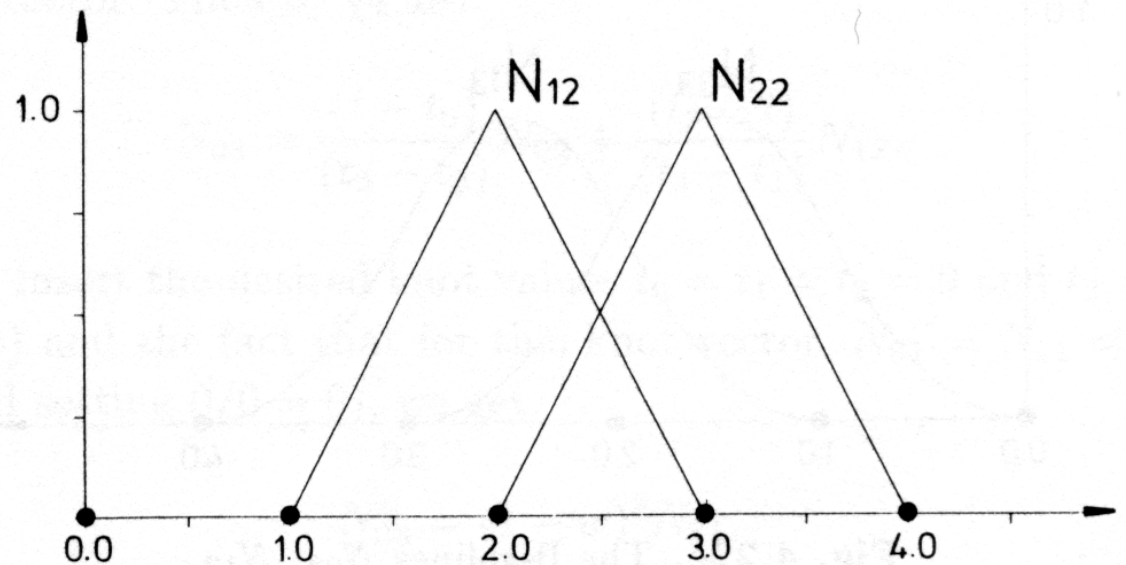
$$B_{k,d}(t) = \left( \frac{t - t_k}{t_{k+d-1} - t_k} \right) B_{k,d-1}(t) + \left( \frac{t_{k+d} - t}{t_{k+d} - t_{k+1}} \right) B_{k+1,d-1}(t)$$

- Division by 0 gives 0



**Fig. 4.22c.** The B-splines  $N_{01}$ ,  $N_{21}$ .

These figures show  
blending functions with  
a uniform knot vector,  
knots at 0, 1, 2, etc.  
Note that  $N$  is the same as  
our  $B$



**Fig. 4.22d.** The B-splines  $N_{12}$ ,  $N_{22}$ .